



Trade Science Inc.

December 2008

Volume 4 Issue (2-3)

Macromolecules

An Indian Journal

Full Paper

MMALJ, 4(2-3), 2008 [131-134]

Internal friction of polymer composites with nanosilicas fabricated by ultraviolet irradiation

Xu Guo Cai*, Xiing Hong Long, Ji Xiao Li, Tan De Xin

Department of Chemical Engineering, Anhui University of Science and Technology, Huainan 232001, (P.R.CHINA)

E-mail : gcxu@aust.edu.cn

Received: 20th April, 2008 ; Accepted: 25th April, 2008

ABSTRACT

The internal friction behavior of the nanocomposite polymer was studied using a Multifunction Internal Friction Apparatus. It is shown that the internal friction peak in the polymer has relaxation feature and the peak height is almost independent of frequency for the polymer without nanosilica. Nevertheless, the peak height for the polymer with nanosilica increases not only with increasing vibration frequency, but also with increasing nanosilica content, which results from the stronger interaction between nanosilica with polymer chains. For the nanocomposite polymer with 3wt% nanosilica, the activation energy of polymer chain motion is bigger than that of neat copolymers. © 2008 Trade Science Inc. - INDIA

KEYWORDS

Internal friction;
Polymer;
Nanocomposite;
Silica.

1. INTRODUCTION

The experimental methods of investigating polymeric systems nowadays have reached a very developed stage, which allows micromanipulation up to the level of single monomers. In this way, information on basic macroscopic features, such as the mechanical module and the dielectric relaxation, gets complemented by observations on the microscopic level; Furthermore one can monitor the motion of portion of the macromolecules through some special methods.

The internal friction method has been widely used to investigate the various low frequency relaxation processes of solid materials in recent decades^[1]. However, all the previous investigations, to our knowledge, are almost focused on low damping metal materials, such as neat metal or alloys^[2], nonmetal composites and so on, and there has been very little research concerning

for organic polymers, especially composite polymer^[3]. It is well known that polymers are complicated systems that display a rich variety of dynamical processes in the time/frequency scale-with vibrations, and the dynamical process has something to do with side-group motions, α -transition, secondary relaxations, segmental dynamics. The internal friction method can be used to determine above-mentioned the dynamical processes in polymers such as the glass transition, obtaining some information on the microstructure of polymer.

Nanosize silica is a very useful reinforcement of thermoplastic and thermosetting polymers if it can be dispersed well in polymer matrixes^[4-7]. However, the structure complex of the multicomponents of the composite polymers increases the insufficiency for understanding the relationships of microstructures and components with dynamical properties of polymer composites containing nanometer scale fillers. Therefore, it is necessary to

Full Paper

investigate the relaxational features of composite polymers by internal friction method for understanding the microscopic reinforcing mechanism of nanosize silica.

2. EXPERIMENTAL

The specimens used for measuring internal friction are prepared from biphenyl A epoxy diacrylate as the oligmer, butyl acrylate and methyl methacrylate as active monofunctional monomer, Irgacre 907 (2-methyl-1-(4-methylthiophenyl)-2-morpholinopropanone-1) as photoinitiator, and Silica with a size of 10-15 nanometers as additive components. All chemical reagent were used as-received from market.

After the solid powder silica were added with a certain proportion (all wt %) to liquid active components containing oligmers (about 20-50%), monomers (45-75%), and photoinitiator (3%), the mixtures were stirred by a mechanical stirrer and a supersonic vibrator at room temperature for nearly 1 h to get stable dispersing systems. Then the dispersing mixtures, poured into sample cells to obtain $1 \times 5 \times 55 \text{ mm}^3$ specimens, was photopolymerized on a UV curer (UV125, Beijing Expoit Co.) by the irradiation of high-pressure mercury lamps with a UV intensity of $0.4 \text{ m W} \cdot \text{cm}^{-2}$ for less than 1 min to obtain solidified nanocomposite samples for testing.

Microstructures of the nanosilica composites materials were characterized on the cut samples utilizing standard operating techniques. The cut samples, into which the bulk nanocomposites were cut at the ambient temperature by diamond knife and the cut were collected on a copper grid, were observed by means of transmission electron microscopy (TEM) with a Model of JEOL JEM100SX.

All samples were shaped to cuboid with $1 \times 5 \times 55 \text{ mm}^3$ and polished to meet the need of the measurements of the low-frequency internal friction. The internal friction (Q^{-1}) and relative shear modulus were measured by a Multifunction Internal Friction Apparatus (MFIFA-1, Institute of Solid State Physics, Academia Sinica)^[8], which basically consists of an inverted torsion pendulum, a temperature programmer a photo-electron transformer, an IBM computer and an 8087 processor for controlling all measurements. This apparatus could provide several different frequency mea-

surements at one temperature running in the forced oscillation mode. The scope of temperature measurement ranged from 240K or 300K to 390K. During running, the specimen was oscillated at several discrete frequencies in sequence, and was heated at a rate of $1^\circ\text{C}/\text{min}$.

3. RESULTS AND DISCUSSION

Figure 1 shows internal frictions-temperature curves of the neat polymer without nanosilica. It can be seen that the neat copolymers presents an internal friction peak at about 320 K and the peak position shifts toward higher temperature with increasing frequency, indicating that the peak possessed relaxational feature.

For a thermal activation relaxation process, peak temperature and its activation energy follows Arrhenius law^[9], i.e.

$$\tau = \tau_0 \exp(H/kT) \quad (1)$$

where τ_0 is the pre-exponential factor (or the relaxation time at infinite temperature), T is the absolute temperature, H denotes the activation energy, and k is the Boltzmann constant. It is well known that at the peak position the condition $\omega\tau=1$ is fulfilled, where $\omega=2\pi f$ is the angular frequency of measurement, f is vibration frequency. At the internal friction peak position, Arrhenius law can be expressed as follows:

$$\ln \omega = -\ln \tau_0 - H/kT \quad (2)$$

where T is a temperature corresponding to maximum value of internal friction-temperature curve at any frequency. In terms of peak temperatures at different frequencies, the Arrhenius plot ($\ln \omega$ versus $1/T$) can be obtained, as shown in figure 2. From the slope and intercept in figure 2, the activation energy H_1 and the pre-exponential factor τ_{01} can be calculated to be $2.50 \pm 0.5 \text{ eV}$ and $1.34 \times 10^{-36} \pm 4 \text{ s}$, respectively. Abnormal pre-exponential factor may be attributed to the movement of chain cluster but single chain. The present internal friction peak is not standard Debye peak. The calculated activation energy is so high that the stability of polymer composites was subject to disbelieving, so the results can be showed that it is appropriate to apply Arrhenius law to the internal friction peak of metal materials but organic polymer composites.

From figure 1, it can be known that their peak

heights are almost independent of frequency. The internal friction peak possibly results from the movements of the chains in copolymer. There are side chains and different structure main chains. The chains can move and produce an internal friction peak under stress-induced. Because the interaction between molecules or/and segments is equal to each other statistically within copolymers, the internal friction value with different frequency is almost same.

As shown in figure 2, for the nanocomposite polymer with 3w% nanosilica and neat copolymer, H_2 and H_1 can be also calculated to be $2.94 \pm 0.52\text{eV}$ and $2.50 \pm 0.5\text{eV}$, respectively. Obviously, the active energy of composite and neat polymers is too high to stabilize the polymers. Therefore, the application of Arrhenius law to the internal friction peak of organic polymer is probably appropriate. But the relaxation parameter was available to understand the motion of polymer chain. It is deduced from the relaxation parameter that interaction of nanosize particle with polymer chain is of importance very much in thermal relaxation of polymer microstructure.

Figure 3 shows the internal friction-temperature curves of the composite polymer with 3 (wt)% nanosilica at different frequencies. It can be seen that the peak temperature also shifts to higher temperature with increasing frequency. Different from figure 1, the peak heights in figure 3 increase drastically with increases with increasing frequency. The existence of "crosslinking" points resulting from interaction of nanosilica with polymeric chain causes the movable segments shorter, the segments motivation might be trailed off by the "crosslinking" points. In the nanocomposite, the peak temperature from every frequency was higher than that in the neat copolymers, indicating that the presence of the nanometer silica in the polymer matrix improved the thermal stability of materials. By nonlinearly fitting, the relationship of the peak height with frequency can be expressed as:

$$Q_{\max}^{-1} = Ae^{\frac{\omega}{12\pi}} \quad (3)$$

where Q_{\max}^{-1} is the peak height and A is constant, being related to the features of composite polymer. From equation (3), it can be seen that relaxation strength increases exponentially with increasing frequency in the nanocomposite polymer but in the

neat polymer.

Figure 4 shows the internal friction-temperature curves of the composite polymer with different nanosilica content at 0.05 Hz. From figure 4, it can be seen that the height of internal friction peak increases with increasing nanosilica content in the matrix, and the peak temperatures are nearly same for different nanosilica content. This phenomenon results from the stiffening of the matrix imparted by inorganic nanometer silica. The motion of the acrylates copolymer chain was further restricted by the interaction of between polymer segment and silica size. The relaxation strength increases with increasing nanosilica content.

The damping in composition polymer could be attributed to the interaction of the nanosilica inside the polymer matrix with polymer segments. The increase of relaxation strength of the nanocomposites results from the existence of nanosilica in polymer matrix, which results in partial transformation of "free" macromolecule segments into a "bound" state with super-segmental order. As a result, intensification of the overall damping process was observable. On the other hand, there are phase boundaries between nanosilica with polymer chains. These phase boundaries also attribute the damping because of thermal expansion mismatching between nanosilica and polymers and some interface defects. It has been calculated that interface damping is proportional to the volume fraction of reinforce phase^[10]. Therefore, the damping increases with increasing nanosilica content. As a matter of fact, the damping mechanism of nanocomposite polymer with nanometer scale silicas is quite complicated, which is different from the conventional micrometer scale silica. The interface between polymers with nanometer silica were able to be a gradual penetrating region, i.e. the transitional region, as shown in figure 5. It is concluded that the penetrating group is likely to be hydroxyl group of biphenyl A epoxy group suspending polyacrylates main chains and sil-hydroxyl group on surface of nanosilica. The region possibly attributes to main energy dissipating and increases with increasing nanometer particle volume fraction.

From figure 6, it can be seen that nanosilica are homogeneously dispersed with a narrow size distribution in photopolymerized nanocomposite. The dots in the image locate about from 10 nm to 15 nm, in con-

Full Paper

formance with the primary size of nanosilica that is embedded into the polyacrylates matrix. Due to dispersing states uniformly of nanosilica sizes, the interaction between nanosilica and polymer segments is considered to be equivalence, so polymer segments would be activated at almost same temperature for nanocomposites with different concentration of nanosilica in the photocured matrix. The data had not been recorded regularly in higher temperature for the samples have softened, but the tendency of internal friction changing was apparent. Of course, the molecular mechanism of the polymer-nanofiller interaction cannot be completely understood, but it can be suggested that the fillers can restrict chain mobility by formation of an immobilized polymer shell around the filler.

4. CONCLUSIONS

There is an internal friction peak on the internal friction-temperature curves in the polymer. It can be suggested that the peak results from the movements of chains in polymer. The nanosize filler can affect the dynamics of the relaxation peak of the nanosilica composites that fabricated from acrylate oligomer, monomer and nanometer silica powder under irradiation of ultraviolet light, internal friction-temperature curves illustrate that position of internal friction peak is shifted toward higher temperatures with increasing forced oscillation frequency, and the height increases with increasing nanosize powder within organic polymer matrix. For nanosilica composites, the activation energy of polymer chain motion is bigger than that of neat copolymers and the relaxation time smaller.

ACKNOWLEDGMENTS

The authors are grateful for the key Projects of the Science Research supported from the MOE of China (206064), and further thanks are due to the Natural Science Foundation of Anhui Province (grant: 050440907) and Science Foundation of Education Department of Anhui Province, China (grant:2005kj 015zd).

5. REFERENCES

- [1] Ting sui Ke; Fundamental theory of Internal Friction in Solid States, Science Press, Beijing, China. (2000).
- [2] G.C.Xu, J.Wang, X.L.Ji et al; Journal of Composites Materials, **41(18)**, 2213-224 (2007).
- [3] Qijin Zhang, Liu Wei, Peng Dai; Polymer., **39**, 3787 (1998).
- [4] XU Guo Cai, Ai Yuan Li, Li De Zhang et al.; Journal of Applied Polymer Science., **90**, 837 (2003)
- [5] F.Yang, Y.C.Ou, Z.Z. Yu; J.Appl.Polym.Sci., **69**, 335 (1998)
- [6] K.Chanvoot, L.W.James; J.Appl.Polym.Sci., **78**, 1551 (2000).
- [7] E.Sakai, J.Sugita; Cement and Concrete Research, **25**, 127 (1995).
- [8] Ting Sui Ke; Advances in Mechanics, **24**, 336 (1994).
- [9] A.S.Nowick, B.S.Berry; Anelastic Relaxation in Crystalline Solids, Academic Press, New York, 105 (1972).
- [10] E.Reynaud, T.Jouen, C.Gauthier, et al; Polymer., **42**, 8759 (2001).