



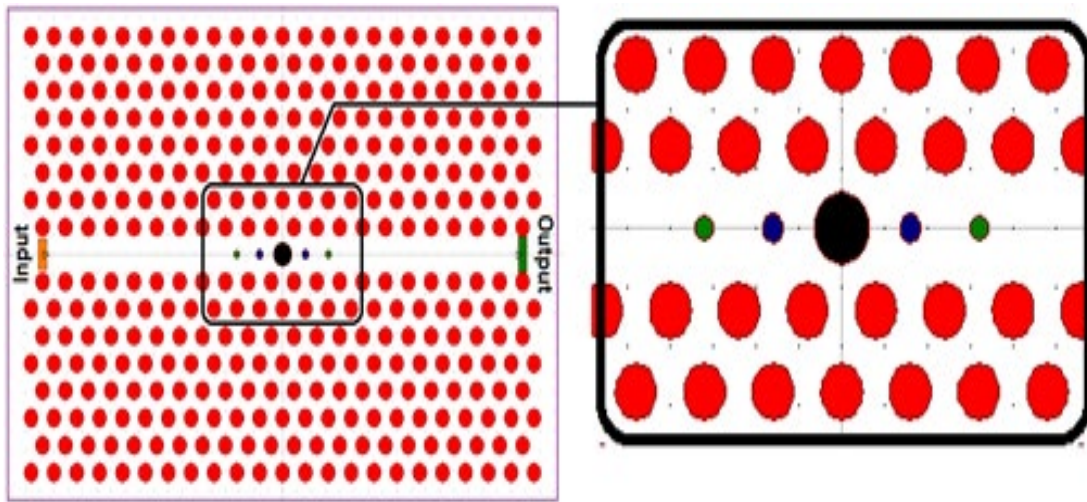




$n_0$  is the refractive index of the medium at zero temperature ( $0^\circ C$ ),  $\alpha$  is the thermo-optical coefficient given by  $2.4 \times 10^{-4}/^\circ C$  for silicon and  $\Delta T$  is the temperature difference [28].

## Results and Discussion

The designed temperature sensor structure of the 2D hexagonal shape based on the resonant cavity is shown in **FIG. 2**. Our sensor is composed of two quasi-waveguides in the horizontal in-line direction, and a resonant cavity is located between them. The in-line quasi-waveguides are created by removing nine silicon pillars for both sides as input and output. The resonant cavity is created by optimizing rays of some internal pillars such as black rods ( $R*1.3$ ), blue rods ( $R*0.5$ ), and green rods ( $R*0.45$ ) placed in the hexagonal array to couple the light signal into quasi-in-line waveguides from the input to the output. The resonance wavelength is observed using the monitor which is placed at the sensor output. The total size of our sensor is  $18\mu m \times 12\mu m$ .



**FIG. 2. Proposed design for the temperature sensor.**

This section describes the optical detection results obtained for the proposed sensor structure. **FIG. 3** shows the electric field distribution of the resonant cavity for the wavelength 1682.1 nm at the output of our proposed device in the temperature range of  $0^\circ C$  to  $500^\circ C$  with a  $50^\circ C$  step size. **FIG. 4** graphically represents the normalized transmission at the output of the proposed sensor at a zero temperature ( $0^\circ C$ ) which corresponds to an intensity of 81.5% at the wavelength 1682.1 nm. On the other hand, the relationship of resonance wavelengths as a function of temperature has been illustrated in **FIG. 5** and recapitulated in the **TABLE 1**. The necessary functional parameters of our designed temperature sensor are compared with the already mentioned sensors, which are summarized in **TABLE 2**. It indicates that the dynamic range, quality factor ( $Q = \lambda_0 / \Delta\lambda$ ), and sensitivity of the proposed temperature sensor are better than those of the previously existing sensor [28-34]. These results are obtained by using the Q-Finder model in RSoft software which is combined by the 2D-FDTD method with fast harmonic analysis to calculate the quality factor Q [35,36].

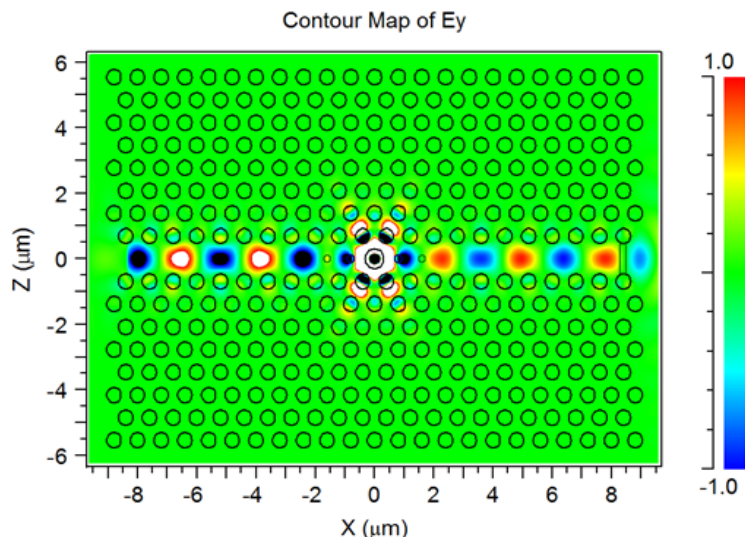


FIG. 3. Electric field distribution of resonant cavity at 1682.1 nm.

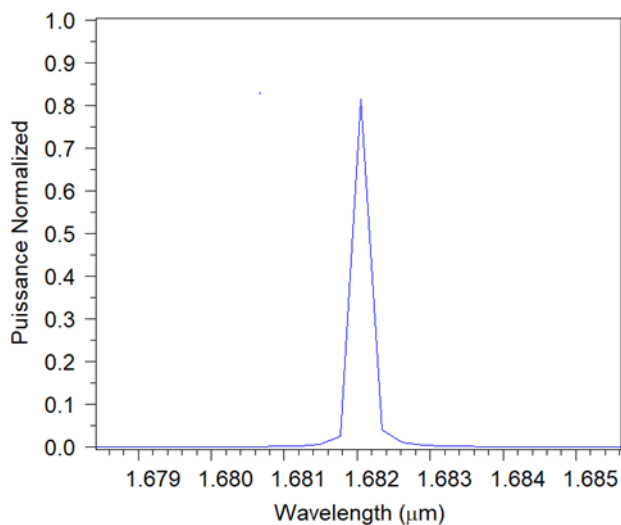


FIG. 4. Resonant wavelength of a resonant cavity at 0°C.

TABLE 1. Functional parameters for the temperature sensor at different temperature levels.

Temperature (°C)	Refractive index (RIU)	Resonance wavelength (nm)	Transmission efficiency (%)	Quality factor	Wavelength shift
0	3.42	1682.1	81.5	17 156	/
50	3.432	1687.5	62	14 688	5.4 nm
100	3.444	1693.2	64.6	12 525	5.7 nm
150	3.456	1698.6	89.6	10 943	5.4 nm
200	3.468	1704.1	92.2	10 182	5.5 nm
250	3.48	1709.7	66.7	10 412	5.6 nm

300	3.492	1714.9	96.8	11 707	5.2 nm
350	3.504	1720.6	98	14 027	5.7 nm
400	3.516	1725.9	50.8	17 234	5.3 nm
450	3.528	1731.6	53	21 105	5.7 nm
500	3.54	1737	50.1	25 349	5.4 nm

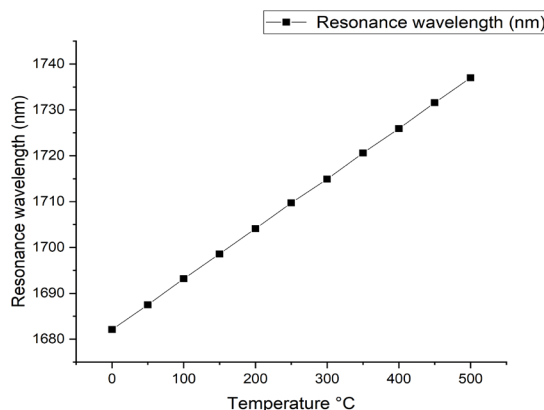


FIG. 5. The linear relation between resonant wavelengths and temperature.

TABLE 2. The proposed functional parameters of the temperature sensor compared with the previous works.

Reference	Dynamic Range (°C)	Quality factor	Temperature sensitivity (pm/°C)
Present work	0 to 500	17 156	109.8
[27]	0 to 100	/	6.6
[29]	25 to 200	214	/
[30]	0 to 450	738.7	59.25
[31]	0 to 80	2506.5	93.61
[32]	20 to 90	/	84
[33]	20 to 70	415.7	88.7
[34]	0 to 360	/	92.3

### Conclusion

In this paper, we presented a two-dimensional hexagonal structure based on the resonant cavity designed for temperature sensing applications. The presence of the thermo-optical effect of the ‘Si’ material plays a very important role in the all-optical temperature sensor. The results of the PWE simulation show that the resonance frequency is shifted to a lower frequency by increasing the temperature. The study of all the functional characteristics of our proposed sensor is realized by using the PWE and FDTD methods. For temperature detection, the resonant cavity structure has a maximum quality factor of 17,156, a very high sensitivity of about 109.8 pm/°C, a dynamic range is 0°C to 500°C, and a size of  $26\mu m^2$ . It is therefore a design that is simple, stable, and

suitable for various applications in integrated optics.

## Acknowledgement

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