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## Synthesis of nanocrystalline Ni-Mn ferrites for magnetic applications by oxalate precursor route

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### ABSTRACT

Manganese nickel ferrite powder with general formula  $Mn_{0.4}Ni_{0.6}Fe_2O_4$  was synthesized through oxalate precursor route. The effect of annealing temperature (400 - 1100°C) on the formation, crystalline size, morphology and magnetic properties was systematically studied. The resultant powders were investigated by thermal analyzer (TG-DTG-DSC), X-ray diffractometer (XRD), scanning electron microscopy (SEM) and vibrating sample magnetometer (VSM). Based on thermal analysis results, the oxalate mixture decomposed thermally in multistep weight loss up to about 680°C. XRD indicated that  $Mn_{0.4}Ni_{0.6}Fe_2O_4$  formed at much lower annealing temperature (=400°C) but contained  $\alpha$ - $Fe_2O_3$  impurity. The hematite phase decreased by increasing the annealing temperature. The lattice parameters and crystalline size were increased with increasing annealing temperature. Single well crystalline ferrite was obtained at 1100°C with crystallite size about 139 nm. The saturation magnetization of the ferrites powders continuously increased with the increase in annealing temperature. Maximum saturation magnetization (44.6 emu/g) was achieved for the formed  $Mn_{0.4}Ni_{0.6}Fe_2O_4$  phase at annealing temperature 1100°C. © 2012 Trade Science Inc. - INDIA

### KEYWORDS

Mn-Ni ferrite;  
Crystal structure;  
Soft magnets;  
Oxalate precursor route;  
Magnetic properties.

### INTRODUCTION

Ferrites, both soft and hard, are used in many technological applications because of their excellent magnetic and electrical properties. Spinel ferrite (soft ferrite) with the general formula  $MFe_2O_4$ , where M = Mn, Co, Ni, Cu or Zn or a mixture of these ions, possess unique electronic or physical structure and chemical stability<sup>[1,2]</sup>. It is an ideal material for high-frequency passive components because of its high permeability, res-

sistivity and permittivity. These materials have been used technologically in magnetic recording media and magnetic fluids for the storage and/or retrieval of information, magnetic resonance imaging (MRI) enhancement, catalyses, magnetically guided drug deliveries, sensors and pigments<sup>[3,4]</sup>. The magnetic properties of these ferrites can be changed by the substitutions of various kinds of  $M^{2+}$  among divalent cations ( $Zn^{2+}$ ,  $Mn^{2+}$ ,  $Ni^{2+}$ ,  $Mg^{2+}$ ,  $Co^{2+}$ ,  $Cu^{2+}$ , ... etc) or by introducing a relatively small amount of rare-earth ions<sup>[5]</sup>. However, the prop-

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erties of these materials are determined by their chemical composition, microstructure and process mechanism. So, the interesting features are that their properties can be enhanced by controlling the chemical composition and the preparation methodology.

Spinel ferrites accommodate cations among two possible available interblaner sublattices namely tetrahedral (A) sites and octahedral (B) sites. Spinel ferrites can be either normal spinel ( $M^{2+}_A[Fe^{3+}Fe^{3+}]_B O_4$ ) or inverse spinel with half of the trivalent ions in the A-sites and the other half together with divalent ions in the B-sites<sup>[6-8]</sup>. Ferrites of similar composition differ in their physical and chemical properties depending on distribution of cations, having different oxidation states, among the available tetrahedral and octahedral sites. Moreover, substitution of magnetic and non-magnetic cations in ferrite materials changes their magnetic and electrical properties<sup>[9,10]</sup>. The change in physical and chemical properties of ion substituted spinel ferrites arises from the ability of these compounds to distribute the cations amongst the available tetrahedral and octahedral sites<sup>[11]</sup>.

Nanocrystalline Ni-Mn ferrite system is one of the most substituted ferrites due to its excellent properties which is mainly applied in electrical devices and in catalyses. The Ni-Mn ferrite ( $Mn_xNi_{1-x}Fe_2O_4$ ) crystallizes in an inverse spinel structure and can be represented by  $(Mn_xFe_{1-x})_A(Ni_{1-x}Fe_{1+x})_B O_4$  where x is defined as the inversion parameter and depends upon preparation conditions and heat treatment<sup>[1, 11-18]</sup>. Spinel nanocrystalline ferrite displays enhanced magnetic and electronic properties by virtue of their unique electronic or physical structure which may be harnessed for technological applications<sup>[2, 4, 19, 20]</sup>. Moreover, some phenomena like modified saturation magnetization, superparamagnetism, metastable cation distributions, ... etc, have been observed in nanoparticles of various ferrites<sup>[21-23]</sup>.

The conventional way to synthesize ferrites, involves the use of high-temperature solid-state reaction between the oxides/carbonates and then annealing at high temperatures (>1200 °C), has some inherent disadvantages. These include chemical inhomogeneity, coarser particle size and introduction of impurities during ball milling. Various soft chemical methods<sup>[24-30]</sup> like mechanical milling, inert gas condensation, hydrothermal reaction, ox-

idative precipitation, sol-gel synthesis and reverse micelle technique are employed for the preparation of nanoferrites. Most of these methods are economically unfeasible for large scale production. The oxalate precursor technique was used for synthesis of ferrites where a single phase of nanocrystalline ferrite powders with homogeneous microstructure, narrow size distribution and uniform shape at low processing temperature can be produced. The oxalate precursor technique uses the carboxylic groups of oxalic acid to chelate the required cations in a proper solution conditions. Chelating metallic ions in solution using oxalic acid allows the formation, after drying, of a solid oxalate precursor with uniformly distributed cations in the required ratio. Relatively low annealing temperatures were required to form the corresponding oxides since all cations are mixed at molecular scale.

In the present investigation, we synthesized a pure  $Mn_{0.4}Ni_{0.6}Fe_2O_4$  ferrite using the oxalate precursor method. X-ray diffraction (XRD), scanning electron microscope (SEM) and a vibrating sample magnetometer (VSM) were utilized in this study. The effect of annealing temperature (400-1100°C) on the formation, microstructure and magnetic properties of  $Mn_{0.4}Ni_{0.6}Fe_2O_4$  ferrites was also investigated.

## EXPERIMENTAL

The oxalate precursor method was applied for the preparation of Mn-Ni ferrite ( $Mn_{0.4}Ni_{0.6}Fe_2O_4$ ). Chemically grade ferric chloride ( $FeCl_3 \cdot 6H_2O$ ), manganese chloride ( $MnCl_2 \cdot 2H_2O$ ), nickel chloride ( $NiCl_2 \cdot H_2O$ ) and oxalic acid as source of organic were used as starting materials. Pre-calculated stoichiometric ratios of ferric chloride, manganese chloride and nickel chloride solutions and containing equivalent amounts of oxalic acid were prepared. The mixture of ferric chloride, manganese chloride and nickel chloride solution was firstly prepared and then stirred for 15 minute on hot plate magnetic stirrer, followed with addition of an aqueous solution of oxalic acid to the mixture with stirring. The solution was evaporated at 80°C with constant stirring rate until dryness and then completely dried in a dryer at 100°C overnight. The dried powder obtained as precursors. Thermal analysis of uncalcined precursor was carried out. The rate of heating was kept at 10°C/min

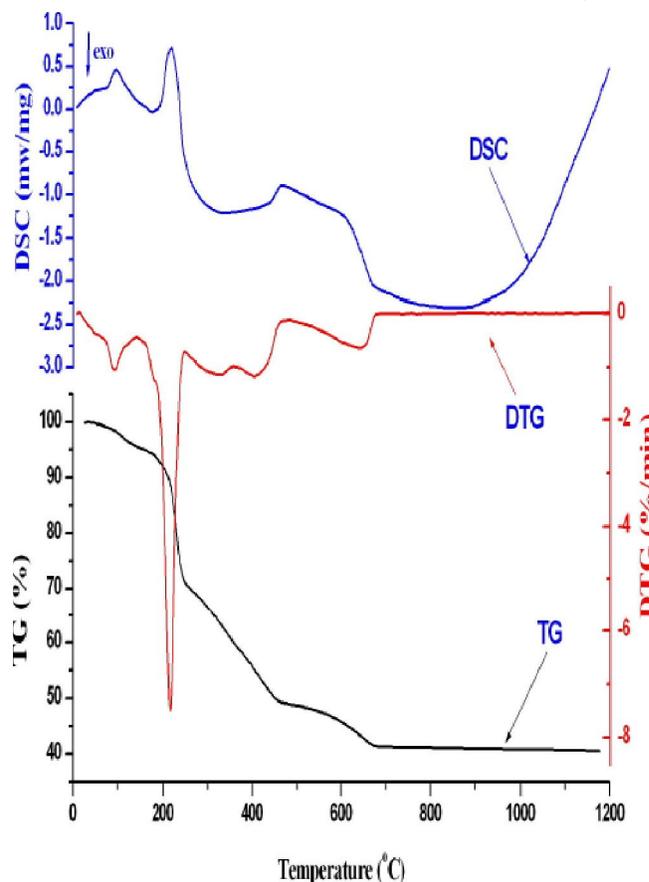
between room temperature and 1200°C. The measurements were carried out in a current of nitrogen atmosphere. For the formation of the Mn-Ni ferrites phase, the dry precursors were calcined at a rate of 10°C/min in static air atmosphere up to required annealing temperatures (400-1100°C) and maintained at the temperature for annealing time 2h.

The crystalline phases present in the different annealed samples were identified by X-Ray diffraction (XRD) on a Bruker axis D8 diffractometer using CuK $\alpha$  ( $\lambda = 1.5406$ ) radiation and secondary monochromator in the range  $2\theta$  from 10 to 80°. The ferrites particles morphologies were observed by scanning electron microscope (SEM, JSM-5400).

The magnetic properties of the ferrites were measured at room temperature using a vibrating sample magnetometer (VSM; 9600-1 LDJ, USA) in a maximum applied field of 10 kOe. From the obtained hysteresis loops, the saturation magnetization ( $M_s$ ) was determined.

## RESULTS AND DISCUSSION

Figure 1 illustrates the thermal analysis profiles (TG-DTG-DSC) obtained during the decomposition of the manganese-nickel-iron oxalates precursors at a heating rate of 10 °C min<sup>-1</sup> in nitrogen atmosphere. The thermal decomposition of the precursor begins as soon as the heating starts. The TG and DTG curves show about 5.2% mass loss upon heating up to 145°C. This mass loss was accompanied by one endothermic peak in the DSC curve at 95°C that could be assigned to the elimination of water from the precursor (dehydration). Major weight loss of 25% mass loss was observed between 150 and 250°C that can be attributed to metal coordinated water molecules<sup>[31]</sup>. This weight loss appeared as endothermic peak in DSC curve at 219°C. By further heating, the decomposition of anhydrous oxalate precursor takes place in multistep weight loss. The sample undergoes exothermic multistep weight loss between 250 and 675°C due to the decomposition of carbonaceous mass of the oxalate precursor. This weight loss was reflected as a broad exothermic peaks in DSC curve at 340 and 670°C. However, the total mass loss was about 59.3% at 675°C which agrees well with a calculated loss of 60.6% for the decomposition of

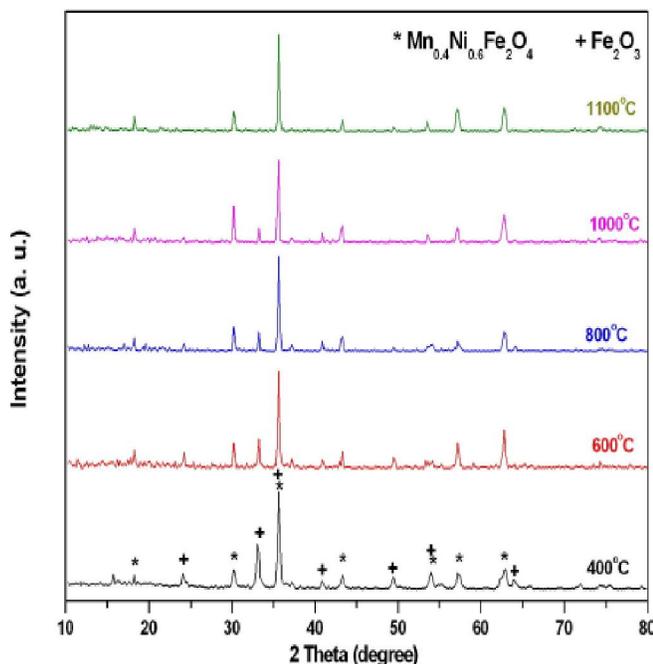


**Figure 1 : Thermal profiles (TG – DTG – DSC) of mixtures of Ni-Mn- Fe oxalates precursors at Fe<sup>3+</sup>/(Mn<sup>2+</sup>+Ni<sup>2+</sup>) mole ratios 2.**

Mn<sub>0.4</sub>Ni<sub>0.6</sub>Fe<sub>2</sub>(C<sub>2</sub>O<sub>4</sub>)<sub>4</sub>.4H<sub>2</sub>O to Mn<sub>0.4</sub>Ni<sub>0.6</sub>Fe<sub>2</sub>O<sub>4</sub>. Beyond 675°C, there was no significant weight loss until 1200°C.

Figure 2 shows the XRD patterns of the calcined powder of Mn<sub>0.4</sub>Ni<sub>0.6</sub>Fe<sub>2</sub>O<sub>4</sub> obtained from manganese-nickel-iron oxalate precursor thermally treated at different temperatures (400 - 1100°C) for 2h. The annealing temperature has a considerable effects on the formation of Mn-Ni ferrite. On the start of the annealing process at 400°C, the formation of single-phase Mn<sub>0.2</sub>Ni<sub>0.8</sub>Fe<sub>2</sub>O<sub>4</sub> could not be obtained at this annealing temperature and, in addition, it contains impurity peaks of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> phase. The patterns consisted of a crystalline cubic Mn-Ni ferrite (JCPDS # 74-2082) phase and a small amount of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> (JCPDS # 80-0599). In this case, the Mn<sub>0.4</sub>Ni<sub>0.6</sub>Fe<sub>2</sub>O<sub>4</sub> is formed at much lower annealing temperature (=400°C). The formation of Mn<sub>0.4</sub>Ni<sub>0.6</sub>Fe<sub>2</sub>O<sub>4</sub> ferrite increased with the rising of annealing temperature as observed from the decrease of peak intensities of the free oxides and the

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**Figure 2 :** XRD patterns of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  from nickel-manganese-iron oxalate precursor treated at different temperatures (400 -1100°C) for 2 h.

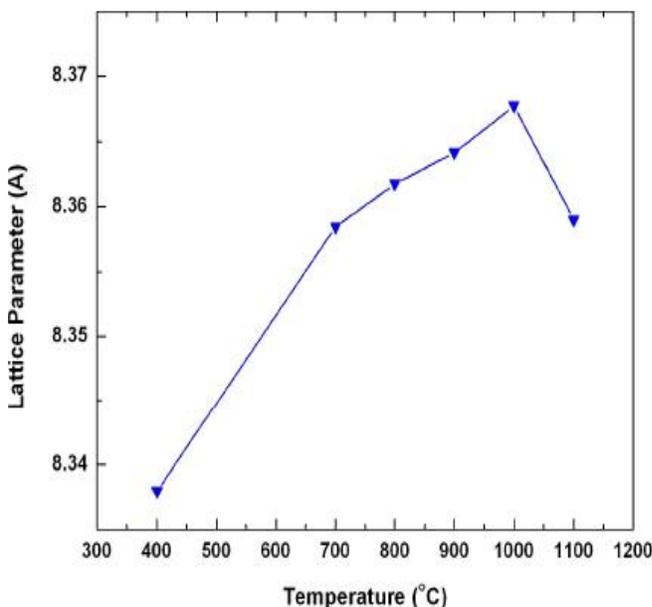
increase of the peak intensities of the formed  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  ferrite. Moreover, a well-crystallized pure single  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  phase was formed at 1100°C. However, no dissociation for the formed ferrite was observed in all annealing temperatures and, on contrast, the formation of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  ferrite increased with rising of annealing temperature. Moreover, a well-crystallized pure single  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  phase was formed at annealing temperature (1100°C). It is reported that at elevated temperatures,  $\text{MnFe}_2\text{O}_4$  is unstable in air and  $\text{Mn}^{2+}$  ions on the surface of  $\text{MnFe}_2\text{O}_4$  firstly oxidize to form  $\text{Mn}^{3+}$  and resulting in the dissociation of the formed  $\text{MnFe}_2\text{O}_4$  [32]. In this work, no dissociation for the formed ferrite in all annealing temperature and instead the formation of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  ferrite increase. This suggests that the substitution of Mn ion in the manganese ferrite with Ni ion stabilizes the  $\text{MnFe}_2\text{O}_4$  phase and decreases the oxidation of  $\text{Mn}^{2+}$  to  $\text{Mn}^{3+}$  in the surface of ferrite. The stability of ferrite increases with the increase of Ni ion content. This is, more or less, in agreement with that observed by Yang et. al.[5]. They found that a single phase of Ni-Mn ferrites can be obtained when the  $\text{Mn}^{2+}$  is smaller or equal to 0.3 mole content.

The lattice parameter for the cubic  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$

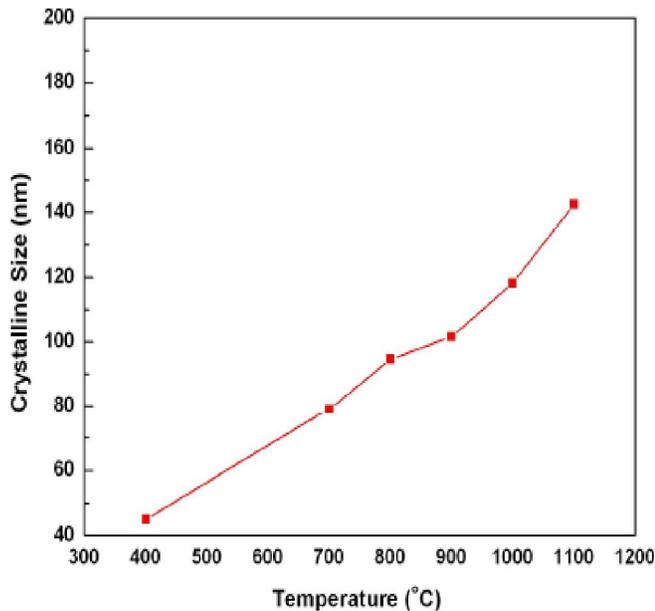
samples annealed at 400, 900, 1000 and 1100°C for 2h as a function of annealing temperature was calculated for the (311) plane using the formula<sup>[33]</sup>:

$$a = d_{hkl} (h^2 + k^2 + l^2)^{0.5}$$

Figure 3 shows the effect of annealing temperature on the lattice parameter of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  powder. The results indicate that the annealing temperature strongly affects the lattice parameter. The value of lattice parameter increases with the increasing of annealing temperature up to 1000°C. Beyond this annealing temperature (1000°C), a decrease in the lattice parameters was found. These results can be due to some structural changes accompanied the formation of manganese ferrite. These changes may be due to the rearrangement of the ions in the ferrite lattice (tetrahedral or octahedral sites)<sup>[34]</sup>. This change of lattice parameter with the change of annealing temperature can be directly influence the magnetic performance of the ferrite. The effect of annealing temperature on the crystalline size of the produced  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  ferrite phase for the most intense peak (311) was determined from X-ray diffraction data using the Debye-Scherrer (Figure 4). As expected, the crystalline size of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  increased by increasing the annealing temperature. The crystalline size for the first single phase obtained at 1100°C was about 138.8nm. However, the crystalline size of the prepared ferrites increased from about 45nm for the ferrite powders produced at annealing temperature



**Figure 3 :** Effect of annealing temperature on the lattice parameters of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  powders annealed for 2h.

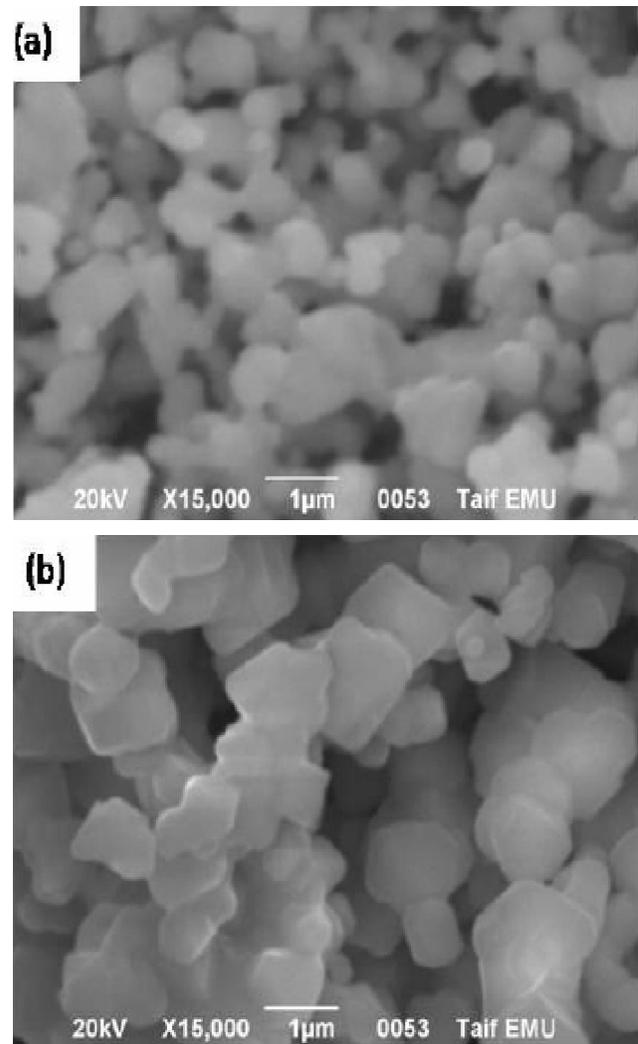


**Figure 4 :** Effect of annealing temperature on the crystalline size of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  powders annealed for 2h.

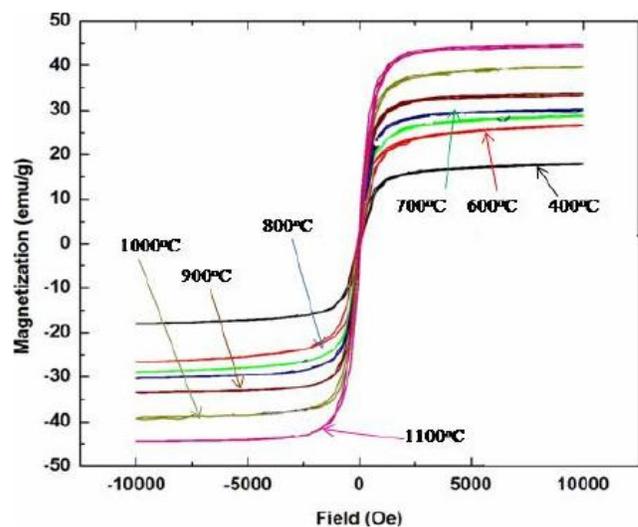
400°C to about 138.8 nm for the powders produced at 1100°C.

Further investigation was carried out by SEM to show the morphology of the particles as synthesized, as well as the development of grain structure. Figure 5 displays SEM micrographs of the effect of annealing temperature (1000 and 1100°C) on the SEM microstructure of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$ . At 1000°C (Figure 5a), the powders possessed irregular microstructures with spherical small particles in addition to a relatively large cubic particles, indicating that the annealing temperature was insufficient for the complete formation of clear crystalline microstructure. The presence of small grains can be attributed to no coarsened  $\alpha\text{-Fe}_2\text{O}_3$  existing in the annealed samples obtained at this annealing temperature. For the powder thermally treated at 1100°C (increase of annealing temperature), the ferrite powders possessed a uniform clear and homogeneous cubic structure as shown in Figure 4b. Moreover, the SEM micrographs showed that the spherical small particles were disappeared at annealing temperatures = 1000°C, which indicated that these temperatures were sufficient to produce a well-crystalline homogeneous microstructure and a uniform size distribution.

The magnetization of the produced  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  ferrite powders was performed at room temperature under an applied field of 10kOe and the hysteresis loops of the ferrite powders were ob-

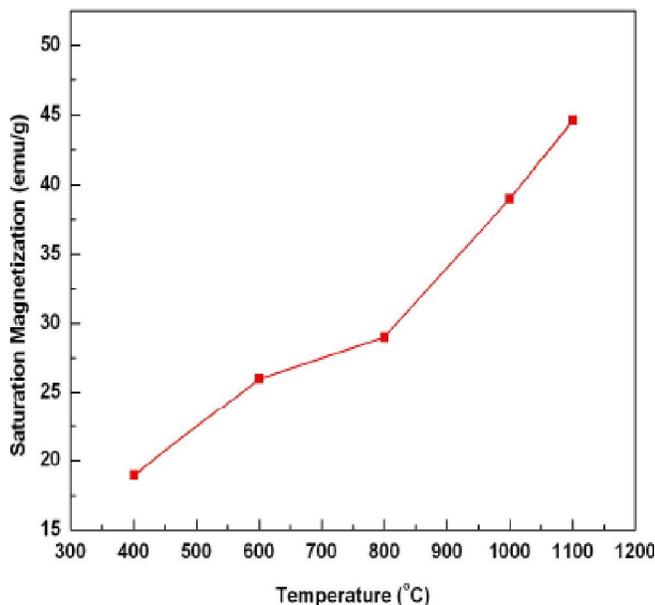


**Figure 5 :** Effect of annealing temperatures on the microstructure of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  annealed for 2h. (a)1000°C (b)1100°C



**Figure 6 :** Effect of annealing temperature on the M-H hysteresis loop of synthesized  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  annealed for 2h.

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**Figure 7 : Effect of annealing temperature on the saturation magnetization of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  powders annealed for 2h.**

tained. Figure 6 Plotted magnetization ( $M$ ) as a function of applied field ( $H$ ) for the effect of annealing temperature while Figure 7 plotted the saturation magnetization of the  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  ferrites powders as a function of annealing temperatures (400 - 1100°C). In general, the produced ferrite was a soft magnetic material due to the deviation from rectangular form and their very low coercivity. There was a large magnetization at 400°C (~19 emu/g) indicating that the  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  ferrite was formed at much lower annealing temperature (<400°C). The magnetization of the ferrite was steadily increased with increasing treatment temperature from 400 (~19 emu/g) to 1100°C (44.6emu/g). Such high saturation magnetization for the synthesized ferrite annealed at = 1000°C can be attributed to the high phase purity and well-defined crystallinity of  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$ . This indicates that the oxalate precursor technique can be used for synthesis of single phase of soft nanocrystalline ferrite powders with homogeneous microstructure, narrow size distribution, uniform shape and a large magnetization at low processing temperature. The increase in the saturation magnetization by increasing the annealing temperature was due to the increase of phase purity and well-defined crystallinity of the ferrite. The crystallite size increased from ~43 nm for the samples annealed at 400°C to ~139 nm for the samples annealed at 1100°C.

## CONCLUSIONS

Nanocrystalline  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  has been synthesized via oxalate precursor route. The effect of annealing temperature on the formation, crystalline size, morphology and magnetic properties were systematically studied. The results showed that:

1. The oxalate precursor of Mn-Ni-Fe mixture decomposed thermally in multistep weight loss up to about 680°C.
2.  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  was started to form at much lower annealing temperature (=400°C)
3. The lattice parameters were increased with increasing annealing temperature up to 1000°C. The average crystalline size increased by increasing the annealing temperature.
4. Single well crystalline ferrite was obtained at 1100°C with crystallite size about 139 nm.
5. The saturation magnetization of the ferrite powders continuously increased with the increase in annealing temperature.
6. The formed  $\text{Mn}_{0.4}\text{Ni}_{0.6}\text{Fe}_2\text{O}_4$  ferrite powders had good soft magnetic properties with maximum saturation magnetization (44.6emu/g) was achieved at annealing temperature 1100°C.

## REFERENCES

- [1] M.Popa, P.Bruna, D.Crespo, J.M.C.Moreno; J.Am.Ceram.Soc., **91**, 2488-2494 (2008).
- [2] S.Son, M.Taheri, E.Carpenter, V.G.Harris, M.E.McHenry; J.Appl.Phys., **91**, 7589-7591 (2002).
- [3] S.Maensiri, C.Masingboon, B.Boonchom, S.Seraphin; Scripta.Materialia., **56**, 797-800 (2007).
- [4] M.Sugimoto; J.Am.Ceram.Soc., **82**, 269-280 (1999).
- [5] H.Yang, L.Zhao, X.Yang, L.Shen, L.Yu, W.Sun, Y.Yan, W.Wang, S.Feng; J.Magn.Magn.Mater., **271**, 230-236 (2004).
- [6] M.M.Hessien, M.M.Rashad, K.El-Barawy, I.A.Ibrahim; J.Magn.Magn.Mater., **320**, 1615-1621 (2008).
- [7] J.A.Toledo, M.A.Valenzuela, P.Bosch, H.Armendariz, A.Montoya, N.Nava, A.Vazquez; Appl.Catal.A., **198**, 235-245 (2000).

- [8] N.M.Deraz, M.M.Hessien; *J.Alloy.Comp.*, **475**, 832-39 (2009).
- [9] S.Kumar, R.Kumar, S.K.Sharma, V.R.Reddy, A.Banerjee, Alimuddin; *Solid State Commun.*, **142**, 706 (2007).
- [10] C.B.Kolekar, A.Y.Lipare, B.P.Ladganokar, P.N.Vasambekar, A.S.Vaingankar; *J.Magn.Magn.Mater.*, **247**, 142 (2002).
- [11] X.Qi, J.Zhou, Z.Yue, Z.Gui, L.Li; *J.Magn.Magn.Mater.*, **251**, 316 (2002).
- [12] M.Naeem, N.Abbas Shah, I.H.Gul, A.Maqsood; *J.Alloy.Comp.*, **487**, 739-743 (2009).
- [13] X.Hou, J.Feng, X.Xu, M.Zhang; *J.Alloy.Comp.*, **491**, 258-263 (2010).
- [14] L.Zhen, K.He, C.Y.Xu, W.Z.Shao; *J.Magn.Magn.Mater.*, **320**, 2672-2675 (2008).
- [15] Y.W.Ju, J.H.Park, H.R.Jung, S.J.Cho, W.J.Lee; *Composites Science and Technology*, **68**, 1704-1709 (2008).
- [16] S.Gubbala, H.Nathani, K.Koizol, R.D.K.Misra; *Physica.B.*, **348**, 317-328 (2004).
- [17] L.Zhao, W.Xu, H.Yang, L.Yu; *Current Applied Physics*, **8**, 36-41 (2008).
- [18] A.S.Albuquerque, J.D.Ardisson, W.A.A.Macedo; *J.App.Phys.*, **87**, 4352-4357 (2000).
- [19] P.C.Fannin, A.Slawska-Waniewska, P.Didukh, A.Giannitoics, S.W.Charles; *Eur.Phys.J.Appl.Phys.*, **17**, 3 (2002).
- [20] M.H.Sousa, F.A.Tourinho, J.Depeyrot, G.J.Da Silva, M.C.F.Lara; *J.Phys.Chem.B.*, **105**, 1169 (2001).
- [21] A.S.Albuquerque, J.D.Ardisson, W.A.A.Macedo, M.C.M.Alves; *J.Appl.Phys.*, **87**, 4352 (2000).
- [22] P.J.Van Der Zaag, P.J.Van Der Valk, M.T.Rekveltdt; *Appl.Phys.Lett.*, **69**, 2927 (1996).
- [23] P.C.Fannin, S.W.Charles, J.L.Dormann; *J.Magn.Magn.Mater.*, **201**, 98 (1999).
- [24] M.Radwan, M.M.Rashad, M.M.Hessien; *J.Mater.Process.Technol.*, **181**, 106-109 (2007).
- [25] H.Sato, T.Umeda; *J.Mater.Trans.*, **34**, 76-81 (1993).
- [26] P.Hu, H.Yang, D.Pan, H.Wang, J.Tian, S.Zhang, X.Wang, A.A.Volinsky; *J.Magn.Magn.Mater.*, **322**, 173-177 (2010).
- [27] J.Huo, M.We; *Mater.Lett.*, **63**, 1183-1184 (2009).
- [28] L.Wang, J.Ren, Y.Wang, X.Liu, Y.Wang; *J.Alloy.Comp.*, **490**, 656-660 (2010).
- [29] J.Ding, W.F.Miao, R.Street, P.G.McCormick, R.Street; *J.Alloys Compd.*, **281**, 32-36 (1998).
- [30] C.Surig, K.A.Hempe, D.Bonnenborg; *J.IEEE Trans.Magn.*, **30**, 4092 (1994).
- [31] P.P.Sarangi, S.R.Vadera, M.K.Patra, N.N.Ghosh; *Powder Technol.*, **203**, 348 (2010).
- [32] H.F.Yu, S.W.Yang; *J.Alloys Compd.*, **394**, 286-291 (2005).
- [33] M.A.Ahmed, S.T.Bishay, S.I.El-Dek, G.Omar; *J.Alloys Compd.*, **509**, 805-808 (2011).
- [34] N.S.Gajbhiye, G.Balaji; *Thermochemica.Acta.*, **385**, 143-151 (2002).